

B602

UNIVERSAL RF BRIDGE

OPERATING INSTRUCTIONS

WAYNE KERR

OPERATING INSTRUCTIONS

for

UNIVERSAL RF BRIDGE B602

THE WAYNE KERR COMPANY LIMITED

ROEBUCK ROAD CHESSINGTON SURREY ENGLAND

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INTRODUCTION

The B602 is an RF Bridge for the measurement of capacitance, conductance, resistance and inductance with an accuracy of 1% at frequencies between 100kHz and 3MHz or, with reduced accuracy, up to 10MHz. The instrument is a passive device and is used in conjunction with an external source and detector.

The bridge is based on the now familiar transformer ratio-arm principle but a novel feature in this case is the inclusion of an inductance standard. This, together with C and R Standards and phase reversing windings on the transformers, permits aperiodic measurements in all four quadrants of the complex plane.

This instrument also introduces a new concept in continuously variable precision voltage dividers that obviate the necessity for variable standards. The device makes use of the magnetic field in a single turn loop and, for this reason, is called a "MAGPOT".

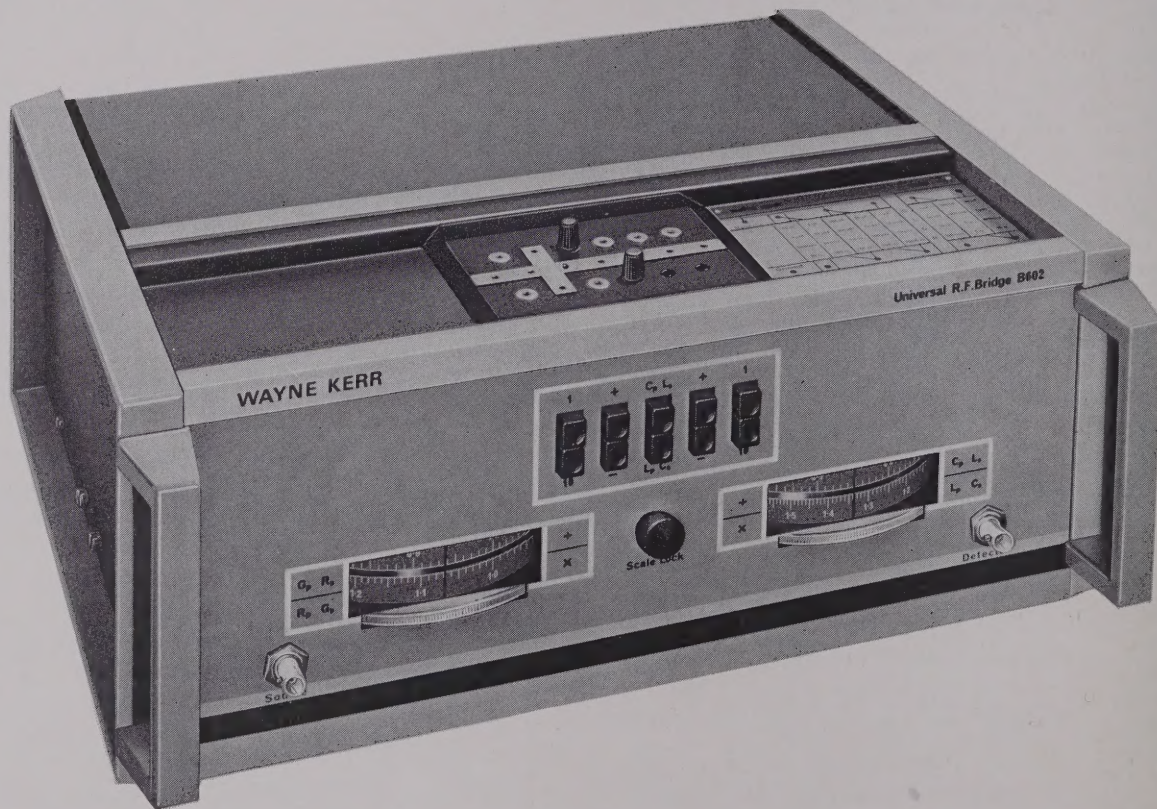
The arrangement of the bridge is such that on the five upper ranges the unknown is measured in terms of its parallel components, while on the lower three ranges the measurement is in terms of the series components.

Certain ancillary instruments and adaptors, described in separate publications, are available for use with the B602; they include the following:

SR268 Bridge Source and Detector, covering the frequency ranges 100kHz to 100MHz in nine bands. The instrument features ganged tuning of Source and Detector, separate attenuators for source output and detector input, visual null detection and it can be operated from either A.C. power line supplies or external batteries.

C602 Coaxial Adaptor permits the use of standard leads with BNC connectors. It also facilitates the use of external transfer standards (for example certain of the Wayne Kerr Q201 standards) for checking the performance of the B602.

The B602 can be supplied either for bench use or as a rack-mounted instrument.



SPECIFICATION

Frequency Range 100kHz – 10MHz

Measurement Ranges Overall:

1fF	–	1mF (0.001pF–1000μF)	} + or –
100μΩ	–	100MΩ	
10pH	–	10H	
10nS	–	10kS	

Accuracy (%)				up to 3MHz	up to 5MHz	up to 10MHz
C	Shunt	1pF	– 10nF*	1	2	5
	Series	10nF	– 1μF†	2	2	5
R	Shunt	10Ω	– 100kΩ	1	2	5
	Series	100mΩ	– 10Ω	2	2	5
L	Shunt	1μH	– 10mH	1	3	5
	Series	10nH	– 1μH§	2	3	5

*Frequency limited to give reactance $\leq 10\Omega$

†Frequency limited, depending on series inductance.

§Frequency limited, depending on self-capacitance of inductor.

Discrimination

(a) Linear Scales

0.1 % of full range capability. One division of these scales represents 1 % of full range capability.

(b) Reciprocal Scales

0.1 % of scale indication. Where a reciprocal scale reading is above 20 it is advisable, where possible, to use the next higher range. If a minor term is being read and the other dial is in full use, then range changing is not possible but, by depressing the 10 button, greater discrimination of the minor term reading can be achieved.

Source/Detector

Wayne Kerr model SR268 (100kHz–100MHz). Detector sensitivity required for 0.1 % discrimination of L, C and R at 1.592MHz for 1V r.m.s. into bridge = 0.3 μ V. Input and output impedances: approx. 75 Ω .

Dimensions (B602)

Width	445 mm (17.5 in.)
Height	165 mm (6.5 in.)
Depth	345 mm (13.5 in.)

Weight

Approx. 11 kg. (24 lb.)

ANCILLARY ITEMS

Source/Detector Leads

D10109/2 (2 off)

Accessories (comprising terminals, link, clip lead and Neutral screen).

OPERATING INSTRUCTIONS

PREPARATION FOR USE

Being a passive instrument, the B602 requires an external source and detector. The most satisfactory results will be obtained when the B602 is used in conjunction with the Wayne Kerr Source and Detector SR268. The SR268 is recommended because it embodies ganged tuning of the source and detector over the full range of frequencies applicable to the B602. Furthermore, being designed as complementary instruments, they stand conveniently together and have terminals arranged for short and direct interconnections. The operating controls for input level and output sensitivity on SR268, and for bridge balancing on B602, fall naturally to hand so that extended periods of operation can be maintained without fatigue. If an alternative source and detector are to be used, the source should provide not less than 2V r.m.s. into 75Ω while the detector sensitivity should be better than $0.3\mu\text{V}$ with 75Ω input impedance. The Wayne Kerr Video Oscillator type O200 is a suitable source and most communication receivers can be used as the detector.

The source and detector should be well screened, both from each other and from the unknown impedance, since any direct coupling between them will cause a false trim. With the detector at maximum sensitivity, there should be no measurable signal when the detector plug is withdrawn from its socket on the bridge and its outer is connected to the outer of the source input connector. When the source and detector are separate units, it may be necessary to connect together the outers of the Source and Detector BNC connectors on the B602.

CONNECTION OF THE UNKNOWN

The Unknown admittance is connected between a pair of terminals screwed into the appropriate holes on top of the instrument according to the approximate magnitude of its major term. The plate to the right-hand side of the terminals gives the full scale value (or equivalent value of unity on the top linear scales) for C, G, L and R. The diagonal lines indicate the full scale values when the terminals so joined are used.

Commencing at the left (as viewed from the front), the function of the terminals is as follows:

The single terminal at the extreme left facilitates connection to the Neutral bar between the two rows of terminals. For some measure-

ments this terminal must be connected to ground at the front terminal of the first pair from the left; a shaped plate is provided for making this connection. The other terminal of this pair is a single-turn "reverse" winding the purpose of which is explained later.

The next three pairs of terminals from the left are the connections for the 'parallel bridge'. The last two pairs of connectors are the 'series bridge' and are used for low impedance measurements. Note that the front connection in both of these pairs is not a screw terminal but a miniature single-pole socket, into which is connected the miniature crocodile clip lead. In the five pairs of bridge terminals, those to the rear are the source or voltage connections while those nearest to the front panel are the detector or current connections.

The channel-shaped bar supplied with the accessories is a screen for reducing the capacitance between the rows of terminals. This screen assists in maintaining the bridge trim and it should be fitted in place for all measurements except those involving the use of a jig or when its presence would hinder the connection of the test component.

When the Unknown cannot be directly connected

to the terminals, standard bridge measurement leads (Type D10065) or low capacity leads (Type D10642B) can be used by means of the Coaxial Adaptor Type C602 (not advised on the lowest impedance range).

SIGN AND MULTIPLIER SWITCHES

The push-button switch block on the front panel facilitates the selection of sign and multiplier for L/C and G/R functions. Selection of the capacitance (C) or inductance (L) standard is made by operation of the central pair of buttons. Note that parallel inductance (L_p) and series capacitance (C_s) measurements are covered by the lower button while the upper button covers parallel capacitance (C_p) and series inductance (L_s) measurements. In general, the most accurate results are obtained when the Unknown is connected to terminals chosen so that the multiplier $\times 1$ is in use. When a $\times 10$ button is operated, scale indications are multiplied by ten for parallel R and L or series G and C but divided by ten for parallel G and C or series R and L. For convenience of reference, these combinations are indicated on the front panel adjacent to the scale apertures.

For most measurements the '+' sign buttons will be operated but cases may arise where the use

of the ‘—’ sign is advantageous, e.g. the additional or alternative measurement of inductance as negative capacitance.

TYPES OF MEASUREMENT

Before the bridge is trimmed, the appropriate ground and neutral connections must be made according to the type of measurement required. These are as follows:

Parallel Measurements

- (a) Small components connected directly to the bridge terminals. Ground and Neutral connected together (Fig. 1).

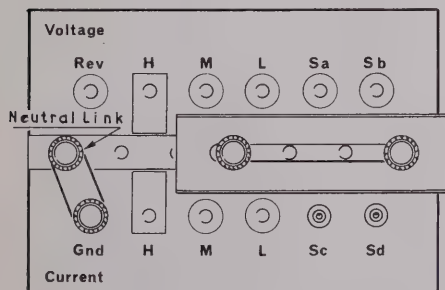


Fig. 1 Neutral Screen and Link arrangement

- (b) Balanced impedances isolated from ground. Ground and Neutral not linked (Fig. 2.)

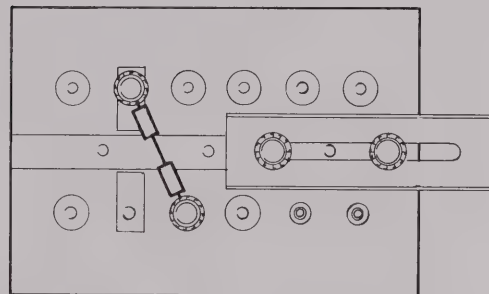


Fig. 2 Balanced Impedances (Floating)

- (c) Balanced impedances with centre point to ground. Ground terminal to centre-point of Unknown; Neutral left free (Fig. 3).

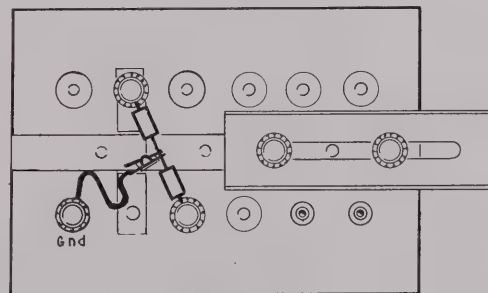


Fig. 3 Balanced Impedances (Grounded)

10 This type of measurement is restricted to the 10Ω and 100Ω ranges; accuracy $\pm 2\%$.

- (d) Unbalanced impedances. Ground terminal to ground of Unknown; Neutral left free.

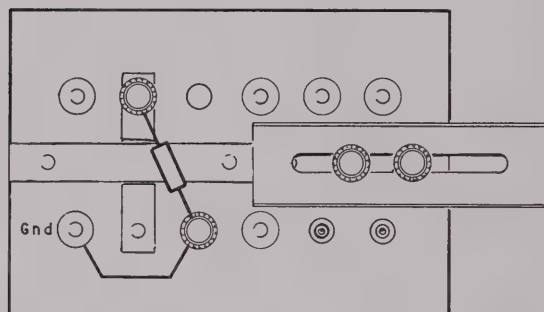


Fig. 4 Unbalanced Impedances (Grounded)

Measurements are then made in the normal manner, except that terminal H, M or L (see Figs. 1 and 4) will be grounded.

- (e) Screened connecting leads. If screened leads are used to connect the Unknown to the bridge terminals (not necessary on lowest impedance range), the screens should be joined at the bridge end and connected to Neutral. Provided that the series impedance

of the leads can be neglected, the only effective impedance is that of the Unknown.

- (f) In-Situ measurements. The arm of the network containing the component to be measured should be connected to the bridge terminals. The shunting effects of associated components can in most cases be eliminated by connecting together the remote ends of these components and taking them to Neutral.

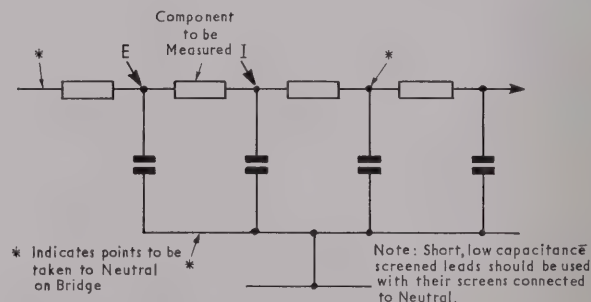


Fig. 5 Measurement of Components In-situ

NOTE: When measurements are made with the bridge Neutral not connected to Ground, the available range is restricted as detailed in the Specification. This restric-

tion is partly due to a falling off of the trim range at higher frequencies and this can be overcome to some extent by using the Reverse terminal as detailed under "Use of the Reverse Terminal" (page 20).

Series Measurements

Such measurements are limited to those in which the Neutral bar is connected to Ground and also to the measurement of components that can be connected directly to the terminal block.

INITIAL TRIMMING (PARALLEL MEASUREMENTS)

- (1) Connect the Source and Detector and tune to the required frequency. Ideally, the bridge should be trimmed at the frequency of operation but, if the trimming is done at 1MHz it will generally hold good between the frequencies 300kHz and 3MHz. For the greatest accuracy the trim should be checked before making the measurement.
- (2) Remove any components connected to the bridge measurement terminals.

- (3) Using the link provided, connect the Ground and Neutral terminals in accordance with the section Types of Measurement. If an adaptor, jig or screened leads are to be used these should be in place.

Press the appropriate sign, multiplier and Cp or Lp buttons.

- (4) Set the two main controls to zero (discounting the 10% scale overlap).

Turn the Scale Lock control clockwise until both scale drums are locked. A slipping clutch allows the thumbwheel controls to be turned independently of the scale drums.

- (5) If the Source and Detector SR268 is being used, refer to the Operating Instructions for that instrument.

If any other source and detector are being used, increase the source output level and detector sensitivity slowly from zero until approximately mid-scale deflection is obtained on the detector indicating meter.

- (6) With the two main scale drums locked at zero, adjust the thumbwheel controls sequentially for minimum detector output, repeating as necessary. Increase the Source output and/or Detector sensitivity as necessary to obtain better balance discrimination and readjust the two thumbwheels as necessary until the final balance condition is achieved.
- (7) Release the Scale Lock control, ensuring that the knob is in the fully counter-clockwise position.

COMPONENT MEASUREMENT (PARALLEL)

Where the approximate value of the component is known, proceed as follows:

- (1) Connect the component or admittance to be measured.
- (2) Balance the bridge with both thumbwheel controls in turn, taking the most significant in each case first.
- (3) Reference to the equivalent value of unity for each scale (as given on the plaque to the right of the terminal block), will give the values of G or R and L or C as appropriate.

Where the approximate value of a component is not known, use the following procedures:

Resistance

- (1) Press the Cp Ls button. Ensure that the conditions of measurement are as specified in the section "Types of Measurement". Trim the bridge as for parallel measurements.
- (2) Connect the component to be measured to Range 4 (see Fig. 7), balance the bridge in the normal way and note the reading on the Rp Gs scale.
- (3) If balance occurs between 10 and 100 on this scale, then the component should be measured on Range 5 for most accurate results.
- (4) If balance on Range 4 occurs just above 100 on the Rp Gs scale then the measurement should be made on Range 6.
- (5) Where a reading closer to infinity is obtained on Range 4, Range 7 or 8 must be used.
- (6) If a balance cannot be obtained, implying that the component is of low impedance, use the Series Ranges as detailed on page 13.

NOTE: In general, the most accurate results are obtained when the Unknown is connec-

ted to terminals chosen so that the multiplier $\times 1$ is in use. When a 10 button is operated, scale indications are multiplied by ten for parallel R and L or series G and C but divided by 10 for parallel G and C or series R and L; these combinations are indicated on the front panel adjacent to the scale apertures.

Capacitance

- (1) Ensure that the conditions of measurement are as specified in the section "Types of Measurement", depress the Cp Ls button, then trim the bridge as for parallel measurements.
- (2) Connect the component to Range 4, balance the bridge and note the reading on the Cp Ls scale.
- (3) If the reading is just below 0.1 use Range 5 for the measurement. If the reading is just below 0.01 use Range 6 and if the reading is close to zero, use Range 7 or 8.
- (4) If a balance cannot be obtained, implying that the component is of low impedance, carry out the measurement on the Series ranges.

Inductance

- (1) Ensure that the conditions of measurement are as specified in the section "Types of Measurement" on page 9. Press the Lp Cs button and trim the bridge in the normal way.
- (2) Connect the component to be measured to Range 4. If the reading on the Lp Cs scale is between 10 and 100, the measurement should be made on Range 5.
If the reading is just above 100 use Range 6 and if the reading is closer to infinity use Ranges 7 or 8.
- (3) Where balance is unobtainable, the component must be measured on the Series (low impedance) ranges as detailed on page 13.

INITIAL TRIMMING (SERIES MEASUREMENTS)

- (1) Connect the Source and Detector and tune to the required frequency. Ideally, the bridge should be trimmed at the frequency of operation but, if the trimming is done at 1MHz it will generally hold good between the frequencies 300 kHz and 3 MHz. For the greatest accuracy the trim should be checked before making the measurement.

- (2) Connect the component to be measured between the Neutral bar and the appropriate terminal in the rear row. Use Range 3 for trimming if component value is not known approximately, and re-trim when the correct range of measurement has been determined as detailed under Component Measurement (Series). Insert the miniature clip lead plug into the socket appropriate to the measurement range required.
- (3) Attach the clip to the component lead connected to the Neutral bar.

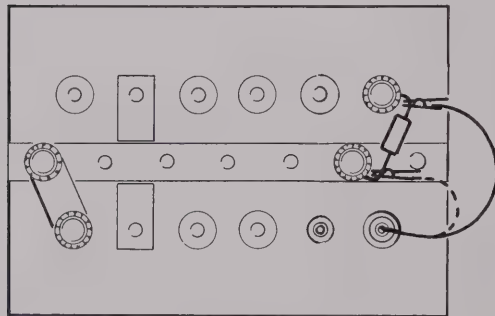


Fig. 6 Component Measurement (Series)

- It should be connected as close to the body of the component as possible unless the component leads are to be included in the measurement. It follows that if the lead impedance forms a significant part of the impedance being measured, this can be included in the measurement by connecting the clip to the appropriate point.
- (4) Using the link provided, connect the Ground and Neutral terminals in accordance with the section "Types of Measurement". If an adaptor, jig or screened leads are to be used these should be in place. Press the appropriate sign, multiplier and Cs or Ls buttons.
 - (5) Set the two main controls to zero (discounting the 10% scale overlap). Turn the scale lock control clockwise until both scale drums are locked; a slipping clutch allows the thumb-wheel controls to be turned independently of the scale drums.
 - (6) If the Source and Detector SR268 is being used, refer to the Operating Instructions for that instrument. If any other source and detector are being used, increase the source

output level and detector sensitivity slowly from zero until approximately mid-scale deflection is obtained on the detector indicating meter.

- (7) With the two main scale drums locked at zero, adjust the thumbwheel controls sequentially for minimum detector output, repeating as necessary. Increase the source output and/or detector sensitivity as necessary to obtain better balance discrimination and readjust the two thumbwheels as necessary until the final balance condition is achieved.

Release the Scale Lock control, ensuring that the knob is in the fully counter-clockwise position.

COMPONENT MEASUREMENT (SERIES)

Where the component value is known approximately, proceed as follows:

With the trim procedure completed, transfer the miniature clip to the other side of the component body, bearing in mind that the component lead impedance can be included in the measurement if so desired. Balance the bridge and note the scale indications.

Where component values are not known, the following procedure should be adopted.

Resistance

Trim the bridge in the normal manner. Connect the component to be measured to Range 3 and balance the bridge.

If the reading on the $G_p R_s$ scale is just below 0.1, carry out the measurement on Range 2. If the reading is less than 0.01 on the scale, make the measurement on Range 1 (See Fig. 7). For maximum accuracy the bridge should be re-trimmed with the component connected to the correct range.

Capacitance

Depress the $L_p C_s$ button and trim the bridge in the normal manner, but without the unknown connected.

Connect the component to be measured to Range 3 (see Fig. 7) and balance the bridge. If the reading on the $L_p C_s$ scale is between 10 and 100, carry out the measurement on Range 2. If the reading is between 100 and infinity use Range 1. The bridge should be re-trimmed on the final range selected to obtain maximum accuracy.

Inductance

Press the Cp Ls button and trim the bridge in the normal manner. Connect the component to be measured to Range 3, balance the bridge and note the reading on the Cp Ls scale. If the reading is between 0.1 and 0.01 use Range 2 and if the reading is between 0.01 and 0 use Range 1. The bridge should be re-trimmed on the final range selected to obtain maximum accuracy.

INTERPRETATION OF RESULTS

On both scale drums the lower scale is calibrated as the reciprocal of the upper scale. Note that the '10' buttons, if operated, are either multipliers or dividers according to the readout scale used—see the section "Sign and Multiplier Switches".

The multiplier buttons operate independently of one another. The value of unity for both scale drums and for each range is given on the plaque to the right of the terminal block. For convenience the plaque is reproduced in Fig. 7, together with a Bridge accuracy table given in Table 1.

When the bridge is balanced, the two scale indications give values for the Unknown in terms of the series components of in-phase and quadrature terms on Ranges 1, 2 and 3.

On Ranges 4–8 inclusive, the scale indications

BRIDGE ACCURACY		
	PARALLEL	SERIES
100kHz– 3MHz	$\pm 1\%$	$\pm 2\%^*$
3MHz– 5MHz	$\pm 2\%$ ($\pm 3\%$ on L)	$\pm 3\%^*$
5MHz–10MHz	$\pm 5\%$	$\pm 5\%^*$

*See "Measurement Accuracy" (Series Bridge)

Table 1 Bridge Accuracy

give the equivalent parallel values of the in-phase and quadrature terms. Either form can be readily converted to the other by means of the following formulae:

$$\left. \begin{aligned} R_s &= R_p / (1 + Q^2) \\ G_s &= G_p (1 + Q^2) \\ C_s &= C_p \left(1 + \frac{1}{Q^2}\right) \\ L_s &= L_p / \left(1 + \frac{1}{Q^2}\right) \end{aligned} \right\} \begin{aligned} & \text{(at 1.592 MHz, } 2\pi f = 10^7) \\ & \text{where } Q = \frac{R_p}{\omega L_p} \\ & \text{or } Q = \omega C_p R_p \end{aligned}$$

$$\left. \begin{aligned} R_p &= R_s (1 + Q^2) \\ G_p &= G_s / (1 + Q^2) \\ C_p &= C_s / \left(1 + \frac{1}{Q^2}\right) \\ L_p &= L_s \left(1 + \frac{1}{Q^2}\right) \end{aligned} \right\} \begin{aligned} & \text{where } Q = \frac{\omega L_s}{R_s} \\ & \text{or } Q = \frac{1}{\omega C_s R_s} \end{aligned}$$

At 1.592 MHz, Q is equal to the ratio of the numerical indication of the C_p scale to that of the G_p scale regardless of the Range in use. For example,

if balance is obtained when the C_p scale indicates 0.8 and the G_p scale indicates 0.4, then $Q = 0.8/0.4 = 2$.

However, if one of the '10' (multiplier) buttons is operated then the appropriate scale indication must be divided by ten before computing Q . At other frequencies, Q is equal to the same ratio but multiplied by $\omega/10^7$.

MEASUREMENT ACCURACY (SERIES BRIDGE)

The Bridge Accuracy for series measurements given in the table on page 16 does not take account of a systematic error inherent in the measurement method used. (See Appendix). The systematic error applicable to each of the low impedance ranges is given in Fig. 8.

To correct for this systematic error the measured value should be multiplied by the appropriate factor given below.

$$\text{True } R_s = \text{Measured Value } R_m \times \left\{ 1 + [(R_1 + R_2) \times R_m / R_1 \cdot R_2] \right\}$$

$$\text{True } L_s = \text{Measured Value } \times \left\{ 1 + [(R_1 + R_2) \times R_s / R_1 \cdot R_2] + [(R_1 + R_2) \times X_{Ls} / R_1 \cdot R_2]^2 \right\}$$

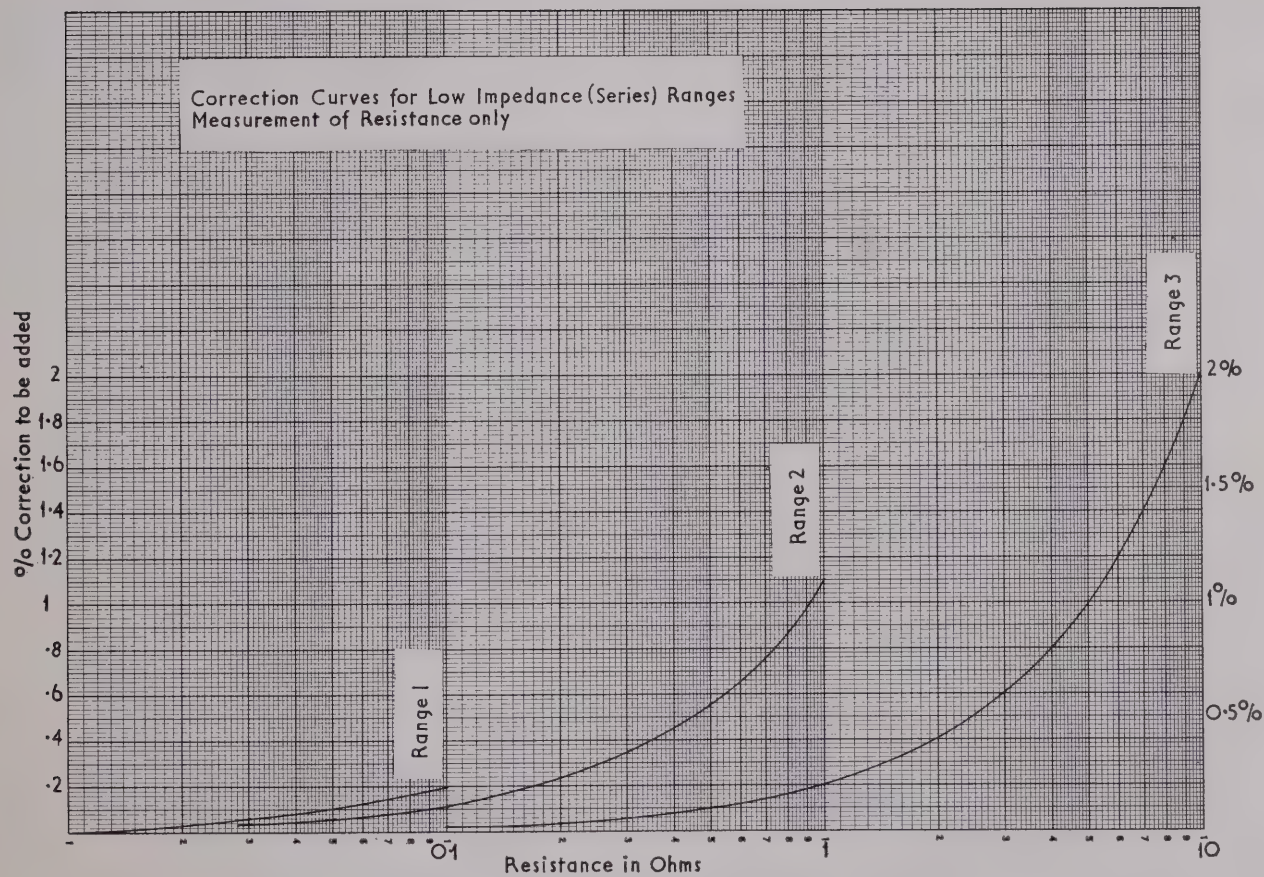


Fig. 8 Systematic Error Correction Curves

$$\text{True Cs} = \text{Measured Value} \times 1 / \left(1 + \frac{[(R1 + R2) \times R_s / R1. R2]}{[(R1 + R2) \times X_{Cs} / R1. R2]^2} \right)$$

where on

$$\text{Range 1 } R1 = 100\Omega \quad R2 = 100\Omega$$

$$\text{Range 2 } R1 = 100\Omega \quad R2 = 1k\Omega$$

$$\text{Range 3 } R1 = 1k\Omega \quad R2 = 1k\Omega$$

USE OF REVERSE TERMINAL

The purpose of the Reverse terminal is to facilitate the connection of external components into the Standard side of the Bridge (parallel measurements only). The reason for doing this is that in some measurements, those involving the use of jigs, for example, it becomes necessary to extend the trim range of the bridge. The normal trim range is approximately $\pm 15\%$ of the range in use; this is adequate for normal use but, on the low capacitance ranges, the self capacitance of a jig may be greater than the trim coverage for these ranges. If, when a jig is used, it is found impossible to trim the bridge, proceed as follows:

- (1) Remove the jig and trim the bridge in the normal way.
- (2) Fit the jig in place, with the connections to the bridge made but no component connected.
- (3) Balance the bridge and note the capacitance

of the jig (it is assumed that the jig capacitance only will be outside the trim range). The capacitance value thus obtained must be neutralised (or trimmed out).

- (4) Select a capacitor of the nearest preferred value to that obtained in (3).
- (5) If the jig capacitance is within the limits of Range 7, the neutralizing capacitor must be connected between the Reverse Terminal and the Current Terminal of Range 7 (i.e. fourth from the left—front row). If measurement is on Range 6, then connect between Reverse and Range 6 Current Terminal.
- (6) With the bridge scales set to 0 and the jig connected, it should now be possible to trim the bridge by following the normal procedure. If more convenient, a small variable capacitor can be used as the neutralizing component. This should be connected between the terminals as described in (5). With the jig in place and the bridge scales at 0, adjust the variable capacitor until balance is obtained. Check the bridge trim by the normal procedure.

The component thus connected takes no further part in the measurement and can be ignored. The above arrangement should hold good for a particular jig on any Range of the bridge but, depend-

ing on the material and construction of the jig, it may not hold good over the full frequency range; as previously recommended, the trim should be checked when the frequency is changed.

APPENDIX

SYSTEMATIC ERROR IN LOW IMPEDANCE MEASUREMENTS

When it is required to measure impedance values below 10Ω , the normal method of measurement becomes impracticable owing to the uncertainty of lead and contact resistances. For the precise measurement of such low impedances a different technique is adopted.

In the normal bridge arrangement, a standard voltage is applied to the unknown and the resulting current is compared with that in a standard impedance. For low values of unknown impedance, i.e. on Ranges 1 to 3 (Low Impedance), the bridge configuration is re-arranged so that Z_u is the shunt element in a T-network (see Fig. 9). If the series elements are made sufficiently large compared with the unknown, the source side of the bridge can be considered as a constant current generator while the detector side functions as a voltmeter. This technique is analysed in Wayne Kerr Monograph No. 1.

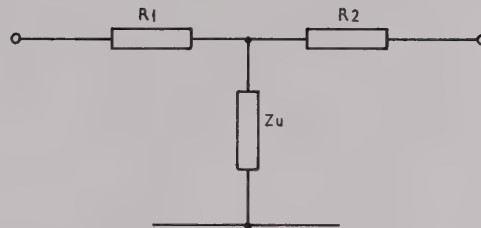


Fig. 9 Measurement Configuration (Series Bridge)

In practice, the series elements ($R1$ and $R2$) are made 100 times greater than the range maximum. This factor would normally give rise to a systematic error of 2%.

Though it was stated above that the source side of the Bridge can be considered as a constant current generator, it will be appreciated that this is strictly so only if the impedance of Z_u is zero; similarly, the loading on the detector is negligible only when Z_u is small compared with the detector input impedance. Since the value of $R1$ is $1k\Omega$ (on Range 3) and the impedance of Z_u can vary between 0 and 10Ω , the maximum error would be 1%; also, since the input impedance of the detector $R2$ is $1k\Omega$ (on Range 3), a further 1% error occurs when the impedance of Z_u is 10Ω .

RECIPROCAL TABLES



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Note: Numbers in difference columns to be subtracted,
NOT added.

	0	1	2	3	4	5	6	7	8	9
1-0	†-00000	99010	98039	97087	96154	95238	94340	93458	92593	91743
1-1	90909	90090	89286	88496	87719	86957	86207	85470	84746	84034
1-2	83333	82645	81967	81301	80645	80000	79365	78740	78125	77519
1-3	76923	76336	75758	75188	74627	74074	73529	72993	72464	71942
1-4	71429	70922	70423	69930	69444	68966	68493	68027	67568	67114
1-5	66667	66225	65789	65359	64935	64516	64103	63694	63291	62893
1-6	62500	62112	61728	61350	60976	60606	60241	59880	59524	59172
1-7	58824	58480	58140	57803	57471	57143	56818	56497	56180	55866
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THE WAYNE KERR COMPANY LIMITED

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